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OPTIMIZATION OF THE ENZYME ASSISTED EXTRACTION OF ESSENTIAL OIL FROM THE LEAVES AND BRANCHES OF *CINNAMOMUM CASSIA* USING BOX-WILSON METHOD

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Abstract. The process of enzyme assisted extraction of essential oil from the leaves and branches of the Vietnamese aromatic plant *Cinnamomum cassia* was studied and optimized using a Box-Wilson central composite design consisting of 05 independent variables (pH, temperature T, time τ , concentration of the enzyme Laccase, and concentration of the enzyme Cellic Htec2), and two dependent variables (reducing sugar and yield of essential oil). Second-order polynomial equations were obtained for the responses, which fitted well with the experimental data. Optimal conditions for oil yield were found at pH = 5.2; T = 44 °C; $\tau = 5h30$ '; Laccase = 0.42 ml/g, and Cellic Htec2 = 1.15 %. The experimental value (0.982 % oil yield) was close to the predicted value (0.978 %). The application of enzyme assisted extraction in combination with optimization using response surface methodology substantially improved the oil yield as compared with traditional method.

Keywords: optimization, Box-Wilson central composite design, enzyme assisted extraction, essential oil, *Cinnamomum cassia*.

1. INTRODUCTION

Cinnamomum cassia (L.) J. Presl (Vietnamese: Quế đơn, English: Chinese cassia or Chinese cinnamon, Family Lauraceae) is a tropical evergreen tree well-known for its bark (cassia bark) and essential oil (cassia oil) which are widely used as spice and aromatic material in food, pharmaceutical, and cosmetic industry, as well as in household. *Cinnamomum cassia* has its origin in Vietnam and is cultivated here since very early time for domestic consumption

and export (China, USA, UK, Germany, etc.). Annually Vietnam produces thousands of tones of cassia bark and up to one hundred tones of cassia oil [1].

Cassia bark is taken directly from the trees after cutting, while cassia oil is traditionally extracted from the leaves and branches by simple hydrodistillation. There is an urgent need in improving the technique to achieve higher oil yield and shorter distillation time. Approaching this need, we have recently been successful in applying the principle of enzyme assisted extraction (EAE) to this process [2]. Through enzymatic treatment of the raw material with a combination of the enzymes Laccase (from *Ganoderma lucidum*) and Cellic Htec2 (Novozyme, Denmark) before distillation substantial improvement of the yield of essential oil and distillation time has been achieved. We also observed in this study that several parameters including pH, temperature, fermentation time, concentration and ratio of enzymes showed significant effects on the outcome of the process and needed to be optimized.

Recently there have been an ever increasing number of reports on successful applications of the response surface methodology for the optimization of processes in chemistry and biotechnology similar to ours [3, 4]. This encouraged us to employ this useful mathematic-statistical tool for the establishment of a statistical model of our above process and the estimation of optimal conditions. For this purpose, the Box-Wilson central composite design, which is a response surface methodology, was used. Five parameters were chosen as independent variables. Two responses, namely, the outcome of total reducing sugar and the yield of essential oil, were chosen as dependent variables.

2. MATERIALS AND METHODS

2.1. Materials

Samples of *Cinnamomum cassia* (L.) J.Presl (Lauraceae) were collected in Van Yen district, Yenbai province. Leaves and branches were dried in the shadow and then finely ground into a powder with a size smaller than 3 mm, packed in polyethylene bags under vacuum, and stored in the dark at room temperature until use.

2.2. Enzyme

The crude Laccase was isolated from culture medium of the fungus *Ganoderma lucidum* (provided by Vietnam Agricultural Genetics Institute). For Laccase production, *G. lucidum* was cultivated in 150 ml fermentation medium in a 500 ml Erlenmeyer flask at 30 °C with shaking at 150 rpm. Fermentation medium was composed of 50 % potato dextrose, 10 g glucose, 2 g MgSO₄·7H₂O and 3 g KH₂PO₄ per liter. Culture broth was then filtered, centrifuged to remove cell biomass (at 10,000 rpm for 30 minutes) and reduced the volume by precipitation with alcohol which was removed to achieve a solution of the crude Laccase. Laccase activity was determined spectrophotometrically by measuring the increase in absorbance at 420 nm, 30 °C using 1 mM ABTS (2,2'-di--azino [3-ethyl-benzothiazolin-sulphonate]) as substrate.

Cellic Htec 2, an enzyme preparation consisting of cellulase and xylanase, was purchased from Novozymes (Bagsvaerd, Denmark).

Enzyme activity was assayed and presented in Table 1.

$\mathbf{N}^{\mathbf{o}}$	Enzymes	Assays	Substrates	Unit	Activity
1	Crude enzymes from G. lucidum	Laccase	ABTS	UI/ml	185
2	Callic Htac?	Cellulase	CMC	III/ml	2800
	Cenic meez	Xylanase	Xylan	01/111	1500

Table 1. Enzyme activities.

2.3. Extraction of essential oil

Essential oil was extracted from plant materials by hydrodistillation. Before extraction, 100 g of cassia leaves and branches powder were subjected to a preliminary treatment by soaking in water for 24 hours (material/water 1:5, g/ml). Then, the material was steam distilled in a 2 1 Clevenger-type apparatus for specified times (2 - 8 hours). The obtained essential oil was dried over anhydrous sodium sulfate and stored in a sealed vial at 10 °C in the dark prior to analysis. Oil yield is calculated based on the mass of essential oil obtained and the mass of the initial material.

Essential oil content (%) = $\frac{\text{Weight of essential oil}}{\text{Weight of raw materials}} \times 100\%$

2.4. Treatment of cassia powder with enzymes

100 g of cassia leaves and branches powder were first pre-treated as described above, then put into a 2 L glass beaker equipped with a hot plate and a stirrer. After adjusting the medium to a pH value of 5.0, specified amounts of enzymes were added (crude Laccase and Cellic Htec2 enzyme). Incubation was then performed under stirring (90 - 120 rpm) at 45 $^{\circ}$ C for 12 hours.

For analysis, 20 mL of the reaction product was taken and centrifuged at 6,000 rpm for 15 minutes. The liquid part was used for the determination of reducing sugars. The contents of reducing sugars in the plant materials before and after the enzymatic treatment were determined by the DNS method as described by Miller (1959), using glucose as reference standard [5].

Mixture of cassia leaves and branches after hydrolysis were then subjected to hydrodistillation for essential oil using a Clevenger apparatus. The essential oil content is determined according to the Viet Nam Pharmacopoeia IV [6].

Essential oil content (%) = $\frac{\text{Weigh of essential oil}}{\text{Weigh of raw materials}} \times 100\%$

2.5. Optimization of hydrolysis

Response surface methodology, in particular the Box-Wilson central composite design [7] was employed to estimate the effect of 5 reaction parameters (pH, temperature, reaction time, Laccase concentration, and Htec2 concentration) on reducing sugar output and yield of essential oil. Procedures for the construction of the 2^{5-1} orthogonal design matrix, for the mathematical-statistical treatments, and for the determination of optimal conditions followed instructions described by Pham Hong Hai (2007) [8]. Regression validation was performed using the Student t-test and the Fisher F-test.

3. RESULTS AND DISCUSSION

3.1. Selection of variables and construction of the design matrix

Based on our prior experiments, 05 reaction parameters, including pH (X_1), temperature (X_2), reaction time (X_3), concentration of the enzyme Laccase (X_4), and concentration of the enzyme Htec2 (X_5), were chosen as independent variables for the design of experiments (Table 2) because of their observed effects on the outcome of the process. The outcome (concentration) of total reducing sugar (y_1 , g/l) and the yield of essential oil (y_2 , % raw material) were chosen as dependent variables.

For statistical calculations the variables X_i were coded as x_i according to Equation (1),

$$x_i = (X_i - \bar{x}_i) / (\Delta x_j) \qquad (i = 1, 2, 3, \dots, k)$$
(1)

where x_i is the dimensionless value of an independent variable, X_i is the real value of an independent variable, \bar{x}_i is the real value of the independent variable at the center point and Δx_j is step change.

		Coded levels										
Variables		-α	-1	0	+1	+α						
pН	(X ₁)	4.23	4.5	5.0	5.5	5.77						
T, ⁰ C	(X ₂)	37.3	40	45	50	52.7						
t, h	(X ₃)	4.91	6	8	10	10.09						
Laccase, ml/g substrate	(X ₄)	0.245	0.3	0.4	0.5	0.555						
Htec2, g/100g substrate	(X ₅)	1.1	1.25	1.5	1.75	1.89						

Table 2. Real values of the independent variables at their corresponding levels in the design.

The chosen 2^{5-1} central composite design matrix (Table 3) consists of 16 factorial points (runs 1 - 16), 10 axial points (runs 17 - 26), and one center point (run 27). The α -value of 1.546 was taken from tabulated data as described by Pham Hong Hai (2007) [8].

In order for the design matrix to be orthogonal, x_j^2 were linear transformed into x_j' by Equation (2).

$$x'_{j} = x_{j}^{2} - \overline{x_{j}^{2}} = x_{j}^{2} - \frac{\sum_{i=1}^{n} x_{ji}^{2}}{N}$$
(2)

Thus, the relationship between the dependent and independent variables in this statistical model was described by a general second-order polynomial equation as follows:

$$\hat{\mathbf{y}} = b'_o + \sum_{j=1}^k b_j x_j + \sum_{u,j=1}^k b_{uj} x_u x_j + \sum_{j=1}^k b_{jj} x'_j$$
(3)

In order to estimate the mean of square of pure error S_{ts}^2 associated with repetition, 03 replicates of experiments at center point were performed, yielding a set of response values of 77.71, 77.71, and 76.62 for y1 and another set of values of 0.972, 0.973, 0.968 for y2. From these data sets, a value of 0.2984 was estimated for S_{ts}^2 of y₁ and a value of 7*10⁻⁶ for S_{ts}^2 of y₂.

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Table 3. Design matrix and experimental results.																									
Run	x ₀	x ₁	x ₂	X3	x4	X5	x ₁ x ₂	x ₁ x ₃	x_1x_4	x ₁ x ₅	x ₂ x ₃	x_2x_4	x_2x_5	x ₃ x ₄	x ₃ x ₅	x_4x_5	, X ₁	, X ₂	, X ₃	, X ₄	, X 5	y1	\hat{y}_1	y ₂	\hat{y}_2
1	+	-	-	-	-	+	+	+	+	-	+	+	-	+	-	-	0.23	0.23	0.23	0.23	0.23	65.208	64.589	0.942	0.938
2	+	+	-	-	-	-	-	-	-	-	+	+	+	+	+	+	0.23	0.23	0.23	0.23	0.23	64.19	65.542	0.953	0.944
3	+	-	+	-	-	-	-	+	+	+	-	-	-	+	+	+	0.23	0.23	0.23	0.23	0.23	67.284	68.322	0.941	0.931
4	+	+	+	-	-	+	+	-	-	+	-	-	+	+	-	-	0.23	0.23	0.23	0.23	0.23	69.598	69.275	0.943	0.937
5	+	-	-	+	-	-	+	-	+	+	-	+	+	-	-	+	0.23	0.23	0.23	0.23	0.23	71.18	71.040	0.946	0.942
6	+	+	-	+	-	+	-	+	-	+	-	+	-	-	+	-	0.23	0.23	0.23	0.23	0.23	71.494	71.993	0.945	0.948
7	+	-	+	+	-	+	-	-	+	-	+	-	+	-	+	-	0.23	0.23	0.23	0.23	0.23	70.588	71.273	0.936	0.935
8	+	+	+	+	-	-	+	+	-	-	+	-	-	-	-	+	0.23	0.23	0.23	0.23	0.23	72.57	72.255	0.947	0.941
9	+	-	-	-	+	-	+	+	-	+	+	-	+	-	+	-	0.23	0.23	0.23	0.23	0.23	72.576	72.090	0.945	0.944
10	+	+	-	-	+	+	-	-	+	+	+	-	-	-	-	+	0.23	0.23	0.23	0.23	0.23	72.89	73.042	0.947	0.950
11	+	-	+	-	+	+	-	+	-	-	-	+	+	-	-	+	0.23	0.23	0.23	0.23	0.23	71.984	72.323	0.936	0.938
12	+	+	+	-	+	-	+	-	+	-	-	+	-	-	+	-	0.23	0.23	0.23	0.23	0.23	73.966	73.275	0.946	0.943
13	+	-	-	+	+	+	+	-	-	-	-	-	-	+	+	+	0.23	0.23	0.23	0.23	0.23	73.88	74.031	0.94	0.949
14	+	+	-	+	+	-	-	+	+	-	-	-	+	+	-	-	0.23	0.23	0.23	0.23	0.23	75.844	74.984	0.951	0.954
15	+	-	+	+	+	-	-	-	-	+	+	+	-	+	-	-	0.23	0.23	0.23	0.23	0.23	74.956	74.273	0.939	0.942
16	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	0.23	0.23	0.23	0.23	0.23	75.27	75.226	0.946	0.947
17	+	-1.546	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	1.62	- 0.77	- 0.77	- 0.77	74.594	72.618	0.962	0.947
18	+	+1.546	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	1.62	- 0.77	- 0.77	- 0.77	75.714	74.091	0.966	0.959
19	+	0	-1.546	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	1.62	- 0.77	- 0.77	74.654	72.362	0.965	0.958
20	+	0	+1.546	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	1.62	- 0.77	- 0.77	76.322	74.078	0.941	0.947
21	+	0	0	-1.546	0	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	1.62	- 0.77	73.27	72.169	0.939	0.948
22	+	0	0	+1.546	0	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	1.62	- 0.77	77.438	77.306	0.969	0.955
23	+	0	0	0	-1.546	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	- 0.77	- 0.77	74.872	71.294	0.93	0.957
24	+	0	0	0	+1.546	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	- 0.77	- 0.77	78.872	78.055	0.976	0.967
25	+	0	0	0	0	-1.546	0	0	0	0	0	0	0	0	0	0	0.23	-	-	-	1.62	77.136	77.749	0.962	0.971
26	+	0	0	0	0	+1.546	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	-	1.62	76.482	77.749	0.965	0.971
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	- 0.77	- 0.77	- 0.77	- 0.77	78.118	77.749	0.976	0.971

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3.2. Mathematic - statistical treatment and validation of the model

Because the design matrix is orthogonal, the coefficients bj and their variances $S_{b_i}^2$ can be directly estimated according to Equation (4) and (5).

$$b_{j} = \frac{\sum_{i=1}^{N} x_{ji} y_{i}}{\sum_{i=1}^{N} x_{ji}^{2}}; j = \overline{1, k}$$
(4)

$$S_{b_j}^2 = \frac{S_{ts}^2}{\sum_{i=1}^N x_{ji}^2}$$
(5)

(7)

Replacing the quadratic terms related to x'_i in Equation (3) using Equation (2) we obtained the normal form of the polynomial Equation (3) as follows:

$$\hat{\mathbf{y}} = b'_{o} + \sum_{j=1}^{k} b_{j} x_{j} + \sum_{u,j=1}^{k} b_{uj} x_{u} x_{j} + \sum_{j=1}^{k} b_{jj} x_{j}^{2}$$
(6)
$$\mathbf{b}_{o} = b'_{o} - b_{11} \overline{x_{1}^{2}} - \dots - b_{kk} \overline{x_{k}^{2}}$$
(7)

Thus,

The software package Design Expert 7.0 was used for the calculations of the established data. The experimental and predicted values were presented in Table 3.

The second-order polynomial Equation (8) was obtained for the dependent variable \hat{y}_1 (reducing sugar outcome) as follows:

$$\hat{y}_{1} = 79.728 + 0.476 x_{1} + 0.555 x_{2} + 1.662 x_{3} + 2.187 x_{4} + 0.439 x_{1} x_{5} - 0.436 x_{2} x_{3} - 0.436 x_{2} x_{4} \\ - 0.689 x_{3} x_{4} - 1.979 x_{1}^{2} - 1.839 x_{2}^{2} - 1.825 x_{3}^{2} - 1.26 x_{4}^{2} - 1.286 x_{5}^{2}$$
(8)

with: $S_{ts}^2 = 0.2984$ as determined above, statistical calculations afforded:

- The estimated variances of the regression coefficients, $S_{b_i} = 0.09001; S_{b_{ui}} = 0.09657; S_{b_{ii}} = 0.16158.$
- The t-values for the regression coefficients, $t_1 = 5.288$; $t_2 = 6.161$; $t_3 = 18.447$; $t_4 = 24.275$; $t_{15} = 4.542; t_{23} = 4.519; t_{24} = 4.519; t_{34} = 7.131; t_{11} = 12.245; t_{22} = 11.381; t_{33} = 11.728; t_{44} = 12.245; t_{24} = 11.381; t_{33} = 11.728; t_{44} = 12.245; t_{44} =$ 7.799; $t_{55} = 7.962$. All t-values were higher than the tabulated value $t_p(f) = t_{0.05}(2) = 4.3$, indicating that the regression coefficients in Equation (8) were significant.
- An F-value of 10.304, which is lower than the tabulated value $F_p(f_1,f_2) = F_{0.05}(13,2) = 19.4$, indicating that the mathematical model was well fitted to the experimental data.

The second-order polynomial Equation (9) was obtained for the dependent variable \hat{y}_2 (oil yield) as follows:

$$\hat{y}_2 = 0.97498 + 0.00285 x_1 - 0.00347 x_2 + 0.00209 x_3 + 0.00328 x_4 - 0.00373 x_1^2 - 0.00833 x_2^2 - 0.00791 x_3^2 - 0.00833 x_4^2 - 0.00394 x_5^2$$
(9)

with $S_{ts}^2 = 7.10^{-6}$; as determined above, statistical calculations afforded:

The estimated variances of the regression coefficients,

 $s_{bi} = 4.3626.10^{-4}$; $s_{bui} = 4.6771.10^{-4}$, $s_{bii} = 7.8253.10^{-4}$.

The t-values for the regression coefficients, $t_1 = 6.528$; $t_2 = 7.954$; $t_3 = 4.785$; $t_4 =$ 7.514; $t_{11} = 4.769$; $t_{22} = 10.647$; $t_{33} = 10.112$; $t_{44} = 10.647$; $t_{55} = 5.031$. All t-values were higher than the tabulated value $t_p(f) = t_{0.05}(2) = 4.3$, indicating that the regression coefficients in Equation (9) were significant.

- An F-value of 17.467, which is lower than the tabulated value $F_p(f_1, f_2) = F_{0.05}(17, 2) = 19.45$, indicating that the mathematical model was well fitted to the experimental data.

Equation (8) and (9) showed that all 05 parameters exert an effect on the output of the process. Furthermore, 3D presentation of the response surfaces described by Equation (8) showed interactions of 4 pairs of parameters. A visual example of interaction between the parameters x_2 (temperature) and x_3 (time) is demonstrated in Figure 1.



Figure 1. Response surface showing interactive effect of temperature (x_2) and time (x_3) .

3.3. Determination of the optimal conditions

As the yield of essential oil is the goal, Equation (9) was used for the optimization of the process. Statistical calculations were performed using an algorithm of flexible tolerance method with the following constraints:

$$\begin{array}{l} -1.546 \leq \ x_{j} \leq 1.546 \ (j=1,...,5) \\ \\ \hat{y}_{1} \geq 70 \ \mu g/ml \end{array}$$

The obtained results afforded the optimum values for each independent variable \boldsymbol{x}_j as follows:

$$x_1^{opt} = 0.384; x_2^{opt} = -0.209; x_3^{opt} = 1.546; x_4^{opt} = 0.192; x_5^{opt} = 0.023$$

The corresponding real values were:

pH = 5.2; T = 44 °C; τ = 5h30'; Laccase = 0.42 ml/g and Htec2 = 1.15 %.

An experiment performed using these parameters gave 78.14 μ g/ml reducing sugar and 0.982% yield of essential oil, which was close to the predicted value (0.978 %).

4. CONCLUSSION

The application of the response surface methodology, in this particular case, the application of a fractional and orthogonal central composite design to construct a statistical model of the process has led to second-order polynomials that fitted well with the experimental data and described in detail the effects of individual parameter as well as their interactive effects. Furthermore, the model enabled a reliable estimation of optimal process parameters. The application of enzyme complex to assist the extraction of essential oil from cassia leaves and branches in combination with the application of the response surface methodology substantially improved the oil yield (41.94% increase as compared with control experiment).

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